

#### Sensitivity Methods in SU2 Continuous Adjoint, Discrete Adjoint, & Finite Difference Methods

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## Introduction

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SU2 provides multiple techniques to calculate sensitivities, or gradients with respect to design variables. They all use the same design variable definitions.

- Finite differences perturb each variable in sequence and re-evaluate the output.
- Continuous adjoint solve the discretized adjoint of the continuous problem and project sensitivities onto the variables.
- Discrete adjoint solve the adjoint of the discretized problem and project sensitivities onto the variables.

This presentation will discuss each of these methods, including description of the shape deformation techniques. Practical application of these techniques will be covered in a following presentation.

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Finite Differences and Shape Deformations

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# Finite Difference Gradient Calculations

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The finite difference method is the most straightforward - the geometry is deformed, the solution is re-evaluated, and the difference of the object function values is divided by the step size. Downsides:

- Requires n + 1 function evaluations for n design variables a cost that becomes prohibitive for large numbers of design variables.
- Accuracy depends on the step size; too large and it will not capture the local gradient, too small and numerical error will effect the gradient accuracy.

Benefits:

- Unlimited number of objective functions can be evaluated simultaneously.
- Simplicity no additional derivations or automatic differentiation needed when addressing a new function.

# Shape Deformations

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A Free-Form Deformation (FFD) box technique is used to achieve smooth shape deformations (Samareh 2004). An initial box surrounding the object to be redesigned is parameterized as a Bézier solid, parameterized by Bernstein polynomials  $B^i$ :

$$X(u, v, w) = \sum_{i,j,k=0}^{l,m,n} P_{i,j,k} B_j^l(u) B_j^m(v) B_k^n(w),$$

where l, m, and n are the orders of the Bernstein polynomials, with one polynomial needed for each of the three dimensions. The control point indices are i, j, and k.



Onera M6 wing with FFD box from the SU2 tutorial on constrained shape design of a transonic inviscid wing at https://su2code.github.io/

# Hicks-Henne Bump Functions

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Hicks-Henne bump functions are use for two-dimensional shape deformations, particularly for airfoil shapes(Hicks and Henne 1978). Hicks-Henne functions are defined in terms of the maximum location  $x_n$ , and result in smooth functions with zero deformation at the end points which can be superimposed to produce more complex deformations.

$$f_n(x) = \sin^3(\pi x^{e_n}), \ e_n = \frac{\log(0.5)}{\log(x_n)}, \ x \in [0,1],$$



NACA 0012 airfoil with a single Hicks-Henne bump on the lower surface deformed by 0.1 with bump centered at 0.3 of the airfoil chord length.

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# Adjoints

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Both the discrete and continuous adjoint methods use calculus of variations-based techniques to compute the sensitivity of a single objective function with respect to infinitesimal changes to the flow solution. These sensitivities are then projected onto specific deformations to the geometry in a post-processing step.

- Execution cost independent of the # design variables.
- Derive new PDE for new functionals.
- Sensitivity of one objective at a time.
- A.k.a.: Lagrange multipliers, co-state problem, or dual problem.

# The Continuous & Discrete Adjoint Method: Literature Review



- Optimal control of PDE systems by (Lions 1971) and (Pironneau 1984).
- ► Developed for aerodynamic optimization by (Jameson 1988).
- (Castro et al. 2007) developed the continuous adjoint for unstructured grids using a surface formulation. (Palacios et al. 2013; Economon et al. 2016) implemented many of these capabilities in SU2.
- Prior to the advent of automatic differentiation tools, analysis by (Nadarajah and Jameson 2000) indicated that the discrete adjoint has both a higher memory requirement and more difficult to implement accurately as compared to the continuous adjoint, while better able to accurately match finite-difference based.
- Details of the discrete adjoint in SU2 using automatic differentiation tools is provided by (Gauger et al. 2007; Albring, Sagebaum, and Gauger 2015; Mader et al. 2008; Zhou et al. 2015).

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J: Function of interest. R: Governing equations.
U: State variables (ex: conservative variables).
S: Design variables/independent variables (ex: surface shape).

 $J(U,S) \qquad \qquad \delta J/\delta S = ?$ R(U,S) = 0





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J(U,S) \qquad \delta J/\delta S = ?

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\delta J = \frac{\partial J}{\partial U} \delta U + \frac{\partial J}{\partial S} \delta S

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\delta J = \delta J - \psi \delta R = \delta U \left(\frac{\partial J}{\partial U} - \psi \frac{\partial R}{\partial U}\right) + \delta S \left(\frac{\partial J}{\partial S} - \psi \frac{\partial R}{\partial S}\right)
```



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choose \psi s.t. \left(\frac{\partial J}{\partial U} - \psi \frac{\partial R}{\partial U}\right) = 0
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                                           \delta J = \frac{\partial J}{\partial U} \delta U + \frac{\partial J}{\partial S} \delta S
                                          \delta R = 0 = \frac{\partial R}{\partial U} \delta U + \frac{\partial R}{\partial c} \delta S
\delta \mathcal{J} = \delta J - \psi \delta R = \delta U \left( \frac{\partial J}{\partial U} - \psi \frac{\partial R}{\partial U} \right) + \delta S \left( \frac{\partial J}{\partial S} - \psi \frac{\partial R}{\partial S} \right)
    choose \psi s.t. \left(\frac{\partial J}{\partial U} - \psi \frac{\partial R}{\partial U}\right) = 0
                              \rightarrow \frac{\delta J}{\delta S} = \left(\frac{\partial J}{\partial S} - \psi \frac{\partial R}{\partial S}\right)
```

# The Adjoint for Fluid Flow



 $\mathcal{R}(U) = 0$  represents the Euler equations.

$$U = \left\{ \begin{array}{c} \rho \\ \rho \vec{v} \\ \rho E \end{array} \right\}, \Psi = \left\{ \begin{array}{c} \psi_{\rho} \\ \vec{\varphi} \\ \psi_{\rho E} \end{array} \right\}$$
$$\min_{S} J = \int_{S} j(U) ds$$
subject to:  $\mathcal{R}(U) = 0$ ,



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$$\min_{S} J = \int_{S} j(U) ds$$

subject to:  $\mathcal{R}(U) = 0$ ,



$$\delta \mathcal{J} = \delta J - \int_{\Omega} \Psi^{\mathsf{T}} \delta \mathcal{R}(U) d\Omega$$

Find  $\Psi$  s.t.  $\delta \mathcal{J}$  independent of all unknown  $\delta U$ .

 $\delta \mathcal{J} = \int_{\mathcal{S}} \left( \frac{\partial J}{\partial \mathcal{S}} (\Psi, U) \right) \delta \mathcal{S} \, ds$ 

# Continuous vs. Discrete Adjoint





# Continuous vs. Discrete Adjoint

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Further detail of continuous adjoint surface formulation included in backup slides

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# Gradient Methods: Pros and Cons



Method	Costs	New Functionals	Accuracy
Finite Differences	Scales with the number of variables.	Just add the new output.	Depends on step size.
Continuous Adjoint	Scales with the number of functionals	Requires implementation of new boundary conditions.	Dependent on well-refined mesh, good implementa- tion.
Discrete Adjoint	Higher memory cost relative to continuous adjoint.	Requires careful coding and recompilation for new functions.	Discretely consistent.

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# Questions?



# Optimization





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Expanding the Lagrangian:  $\delta \mathcal{J} = \delta J - \int_{\Omega} \Psi^{T} \delta \mathcal{R}(U) d\Omega$ , with the assumption that  $\Gamma_{e}$  is undeformed:





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$$\delta J = \int_{\delta \Gamma_e} j(U) ds + \int_{\Gamma_e} \frac{\partial j}{\partial U} \delta U ds = \int_{\Gamma'_e} j(U) ds - \int_{\Gamma_e} j(U) ds + \int_{\Gamma_e} \frac{\partial j}{\partial U} \delta U ds = \int_{\Gamma_e} \frac{\partial j}{\partial U} \delta U ds$$



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Applying the divergence theorem to the second term:

$$\int_{\Omega} \Psi^{\mathsf{T}} \delta \mathfrak{R}(U) d\Omega = \int_{\Gamma} \Psi^{\mathsf{T}} \vec{A} \cdot \vec{n} \delta U ds + \int_{S} \Psi^{\mathsf{T}} \vec{A} \cdot \vec{n} \delta U ds + \int_{S} \Psi^{\mathsf{T}} \vec{A} \cdot \vec{n} \delta S ds - \int_{\Omega} \nabla \Psi^{\mathsf{T}} \vec{A} \delta U d\Omega$$

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Combining the terms above:

$$\begin{split} \delta \mathcal{J} &= \int_{\Gamma_e} \frac{\partial j}{\partial U} \delta U ds - \int_{\Gamma} \Psi^{T} \vec{A} \cdot \vec{n} \delta U ds - \int_{S} \Psi^{T} \vec{A} \cdot \vec{n} \delta U ds \\ &- \int_{S} \Psi^{T} \vec{A} \cdot \vec{n} U \delta S ds + \int_{\Omega} \nabla \Psi^{T} \cdot \vec{A} \delta U d\Omega \end{split}$$

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Combining the terms above: Terms that lead to boundary conditions

$$\delta \mathcal{J} = \left[ \int_{\Gamma_e} \frac{\partial j}{\partial U} \delta U ds - \int_{\Gamma} \Psi^{T} \vec{A} \cdot \vec{n} \delta U ds - \int_{S} \Psi^{T} \vec{A} \cdot \vec{n} \delta U ds \right]$$
$$- \int_{S} \Psi^{T} \vec{A} \cdot \vec{n} U \delta S ds + \int_{\Omega} \nabla \Psi^{T} \cdot \vec{A} \delta U d\Omega$$



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Combining the terms above:

$$\delta \mathcal{J} = \int_{\Gamma_{s}} \frac{\partial j}{\partial U} \delta U ds - \int_{\Gamma} \Psi^{T} \vec{A} \cdot \vec{n} \delta U ds - \left( \int_{S} \Psi^{T} \vec{A} \cdot \vec{n} \delta U ds \right) - \int_{S} \Psi^{T} \vec{A} \cdot \vec{n} U \delta S ds + \int_{\Omega} \nabla \Psi^{T} \cdot \vec{A} \delta U d\Omega$$

Terms that lead to surface sensitivity



Expanding the Lagrangian:  $\delta \mathcal{J} = \delta J - \int_{\Omega} \Psi^{T} \delta \mathcal{R}(U) d\Omega$ , with the assumption that  $\Gamma_{e}$  is undeformed:

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Combining the terms above:

$$\delta \mathcal{J} = \int_{\Gamma_e} \frac{\partial j}{\partial U} \delta U ds - \int_{\Gamma} \Psi^T \vec{A} \cdot \vec{n} \delta U ds - \int_{S} \Psi^T \vec{A} \cdot \vec{n} \delta U ds$$
$$- \int_{S} \Psi^T \vec{A} \cdot \vec{n} U \delta S ds + \int_{\Omega} \nabla \Psi^T \cdot \vec{A} \delta U d\Omega$$

Terms that lead to the adjoint governing equation

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